

# 3D Digitization of Rock Falls for Rock Fall Analysis

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Branch A

Geotechnical Design South 1



# Steps for Rockfall Mitigation

1. Obtain Slope Geometry and Geological Mapping
2. Perform Rockfall Computer Simulation
  - Projectile
  - Probability
  - Energy
3. Design Rockfall Mitigation
  - Rockfall Fences
  - Ditch



# Limitation of Computer Simulation

- Computer simulations have not been calibrated against actual data – actual rockfall
- Fudge factors have been used in simulation
- Generally provides liberal results
  - Recommendations based on Computer Simulation are often under designed



# Research Objectives

- Experiment and develop a rockfall testing protocol and data processing procedure that can
  - Provide reliable data set to be used for site specific model validation
  - Be easily implemented by others
  - Be cost-effective
  - Allow further development and improvement by others





# Rockfall Testing Protocol

- Mark reference points
- Survey slope geometry, reference points and camera locations
- Place at least two synchronized camcorders
- Roll rocks off the slopes
- Measure weight, size of rocks



# Data Processing Procedure

- Synchronize video files
- Calibrate
- Direct Linear Transformation (DLT) method



# Rockfall Test on SR 39

- Test Performed between 10/05/2009 and 10/09/2009
- Four Locations
  - Total Number of Rockfalls:
- Crews
  - Survey Crew from District 7 & HQ
    - Kevin Akin
  - Maintenance Crew from District 7
  - CT Video Team from District 7
    - Steve Devorkin
  - Geotechnical Services
    - John Duffy, Bill Webster, Hung Po Yang, Seungwoon Han, David Jang, Michael Salisbury

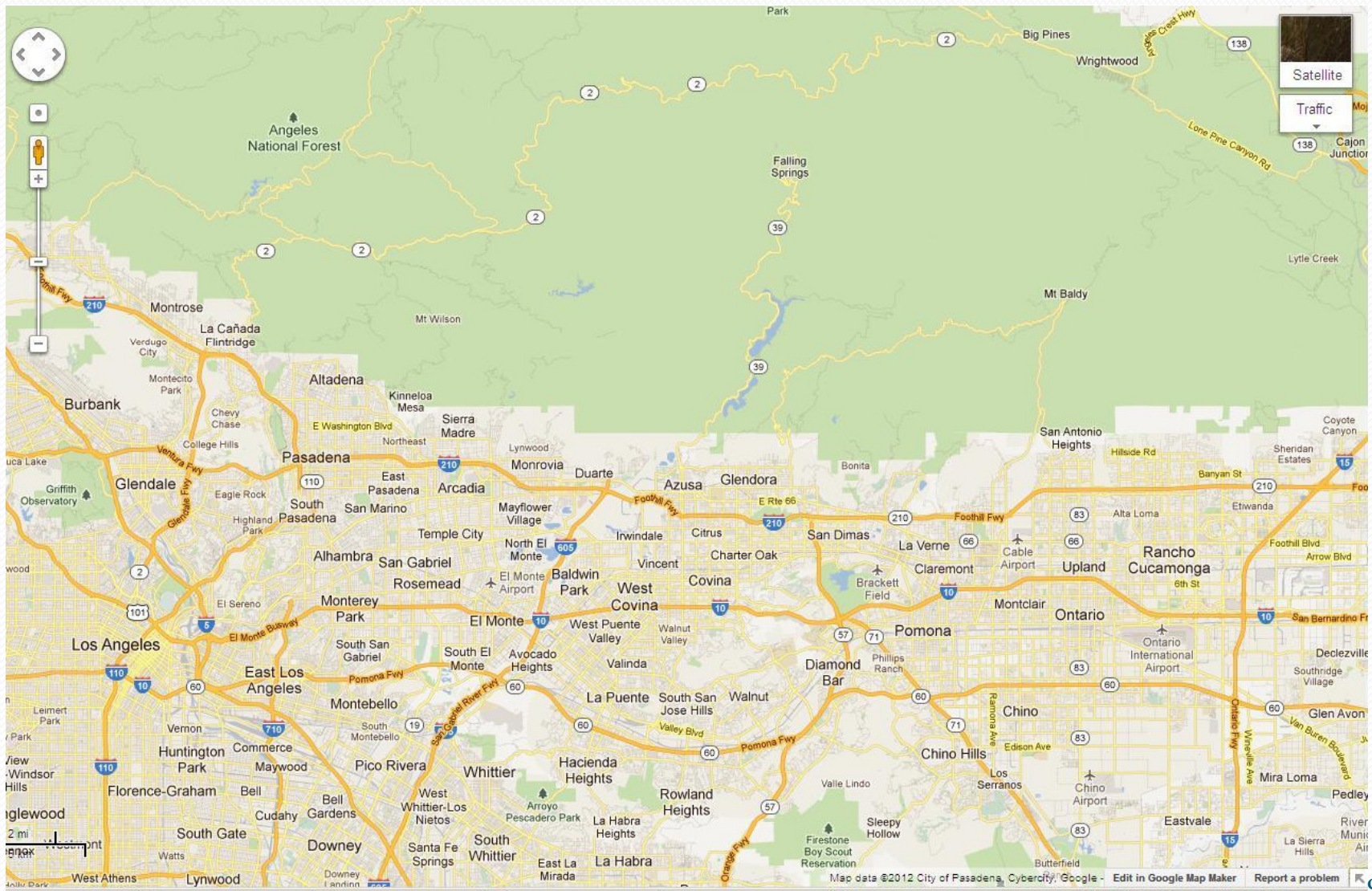


# General Rockfall Concepts

- Hazards from rocks falling from slopes adjacent to roadways
- Caused by gravity, assisted by other mechanisms
- On slopes  $33^\circ$  or steeper
- Evaluation is based on:
  - Maximum Energy Level (M.E.L.)
  - Climate (“Water”)
  - History (“local maintenance”)
  - Risk (decision site distance, speed limit, roadway width, etc.)



# Test Sites





## SR-39

- Narrow two-lane roadway
- located in steep mountainous terrain
- Traverses the west-facing slope of Mt. Islip
- Natural slopes vary from  $20^{\circ}$  to  $40^{\circ}$  from horizontal
- Elevations vary from 5600 ft amsl at the south end of the project to 5900 ft at the north end of the project

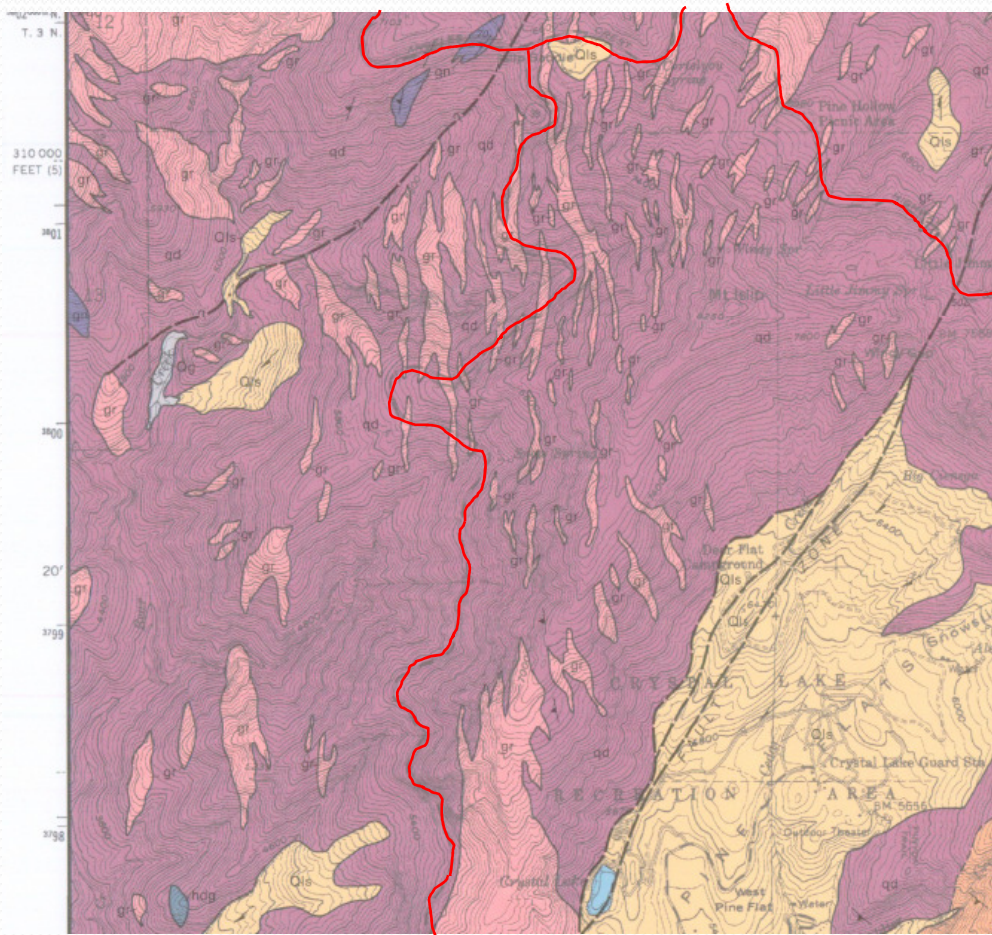




# San Gabriel Mountain Range

- Characterized by deep, v-shaped valleys
- Steep ridges and peaks
- Uplifting at a rate of 3 millimeters per year
- Natural soil cover is very thin along ridges and peaks
- Valleys have thicker soil cover, dominated by boulders & coarse sedimentation from erosion of canyon slopes; may have stream channels
- Sparsely forested; intense precipitation ( ~ 30 in/yr in the project area)
- Severe freeze-thaw conditions with heavy natural erosion

# Geology



Fine-grained Granodiorite:

- Moderately hard
- Intensely fractured
- Moderately weathered

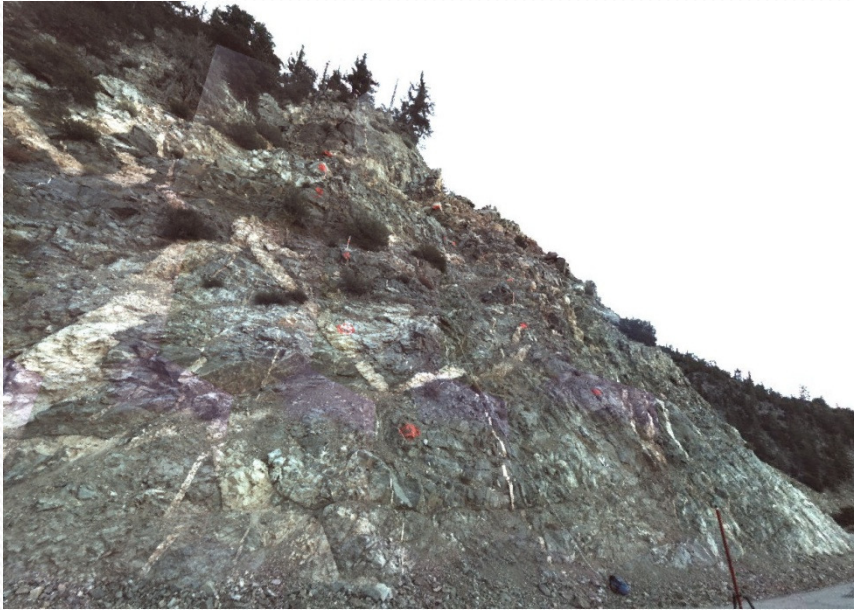
Gray Quartz Diorite:

- Hard
- Slightly fractured
- Slightly weathered

Covered by thin, discontinuous colluvium



# Location 1 (Angle A)



Quartz veins in Gray

Quartz Diorite:

- Hard
- Moderately fractured
- Weathered

Maintenance characterized location as:

- Many rockfalls
- Some were too large to move by truck (~ 6 feet largest diameter)

Slope length ~174 feet

Slope angle  $\sim 53^\circ$

# Location 1 (Angle B)



RHRS score = 408

Proposed Mitigation:

- Cable Drapery
- Standard Barrier
- Hybrid Barrier

More than one proposed mitigation involves a barrier. The geometry of the slope and roadway provide a high score. The risk to motorist in each rockfall event is likely to be very severe.



# Location 2 (Angle A)



Fine-grained Granodiorite:

- moderately fractured to intensely fractured
- hard
- weathered

Maintenance characterized this location as:

- Avalanches in chutes
- Many rockfalls

Slope Length = 140 feet

Slope Angle ~ 55°

# Location 2 (Angle B)



RHRS Score = 308

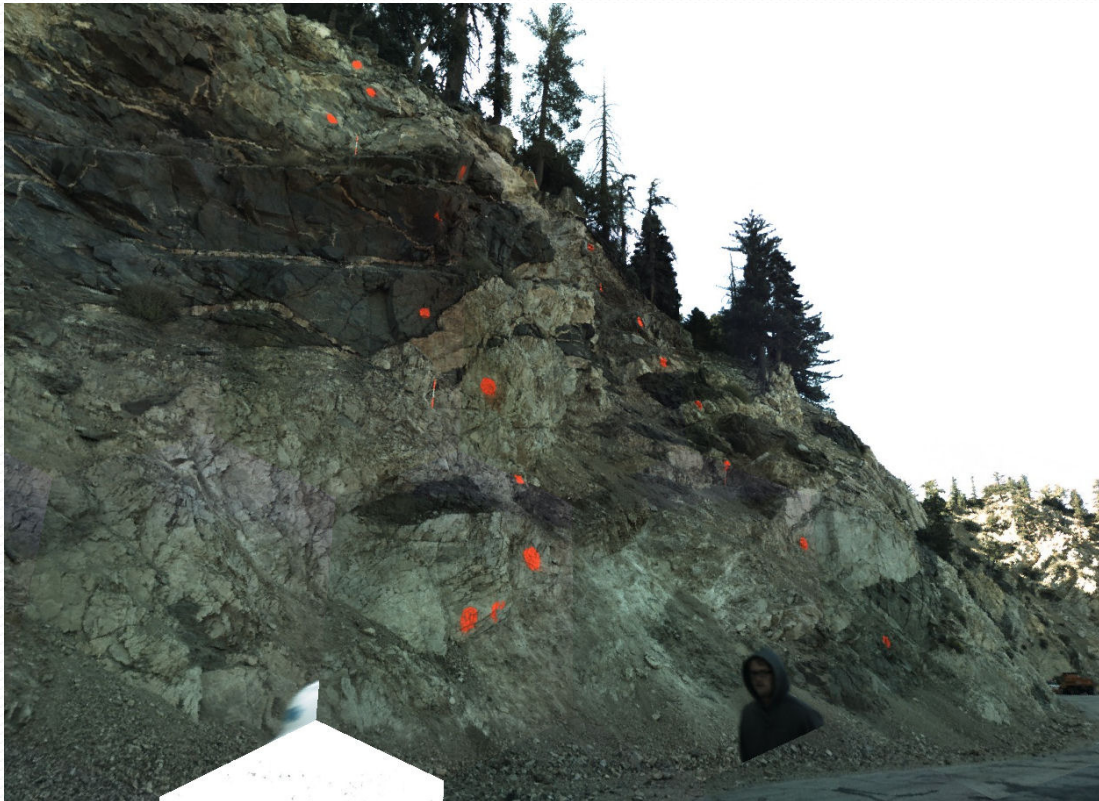
Proposed mitigations:

- Hybrid
- Barrier
- Drapery
- Anchored Mesh

Considered a priority because a standard barrier would potentially mitigate rockfall hazard



## Location 3 (Angle A)



Gray quartz diorite and fine-grained Granodiorite:

- Hard to moderately hard
- Intensely fractured
- Weathered

Maintenance characterized this location as:

- Rockfalls
- Rockslides
- Avalanches in chutes
- Many falls

Slope length ~141 feet

Slope angle ~ 52°

# Location 3 (Angle B)



RHRS score = 421

Proposed Mitigation:

- Hybrid
- Drapery
- Anchored Mesh
- Barrier

Considered a priority because of rockfall history and barrier is a proposed mitigation. Geology and Structure of the slope is different from previous Location 1 & 2.



# Location 4 (Angle A)



Fine-grained Granodiorite:

- Hard to very hard
- Moderately fractured
- Slightly weathered

Maintenance characterized this location as:

- Active rockfall
- Clean ditch frequently

Slope length ~ 143 feet

Slope angle ~ 45°

# Location 4 (Angle B)

RHRS score = 437

Proposed Mitigation:

- Cable Drapery
- Anchored Mesh
- Barrier

This location is a priority due to the high score and maintenance history of persistent rockfall. This slope has similar geology to Location 2 however it has more soil cover.

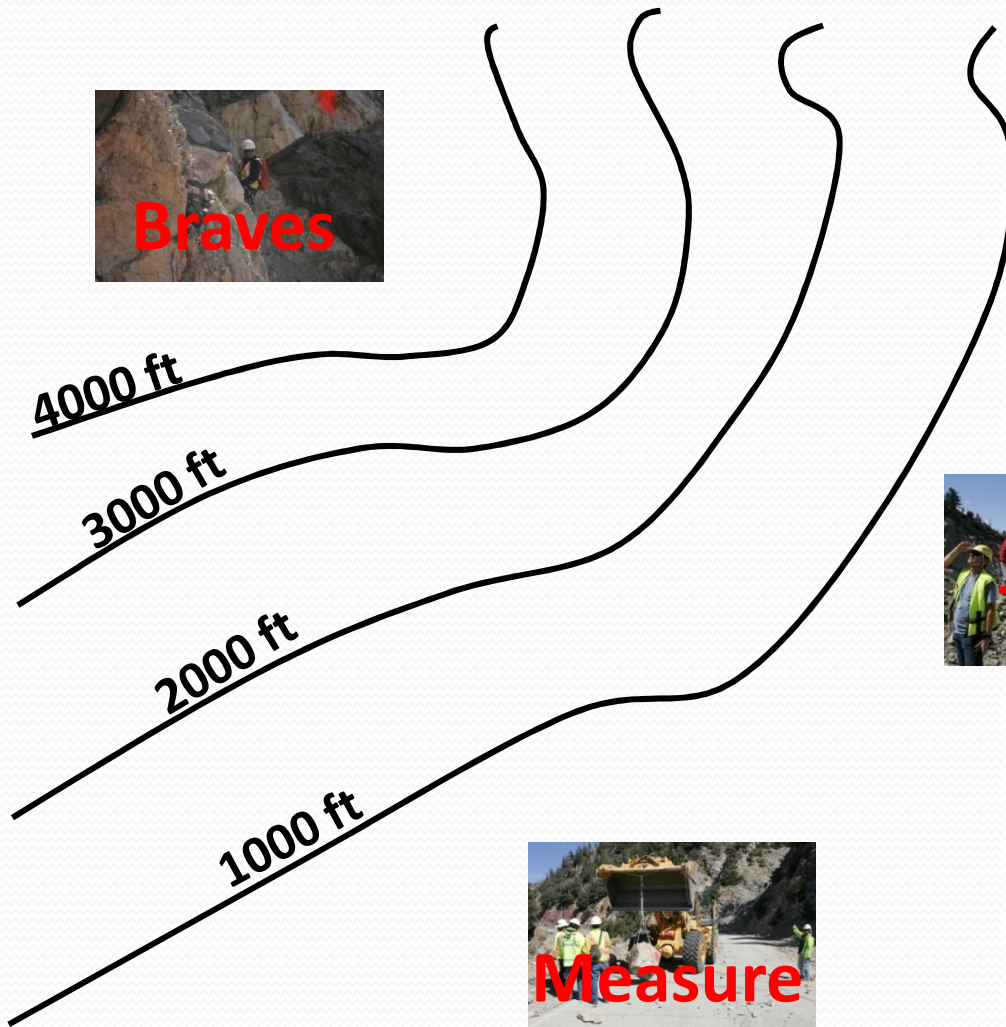






# Rockfall Tests

- Tasks for Each Location/Rockfall
  - Mark Reference Points
  - Survey and LIDAR
  - Roll Rock
  - Record Video
  - Measure (Weight of Rocks and Distance from Edge of Slope)
    - Load cell and rock net
  - Clean-up





# Collected Information

- Survey Data
  - ASCII format data
    - Slope geometry
    - Reference points
    - Camera locations
  - Needs to be visualized
- Video records
  - VOB format
    - Cannot be played in normal CT computers
  - Need to be edited and converted into AVI format

# Outcome

**SITE4.asc - Notepad**

File Edit Format View Help

6606154.556604	1949500.101768	6642.296841	44	236	242	238
6606132.145230	1949648.576603	6527.821309	126	99	101	83
6606131.923340	1949648.521353	6527.684341	132	115	116	94
6606181.493464	1949711.815915	6534.401199	116	72	74	57
6606181.425333	1949711.716605	6534.431035	115	73	75	59
6606187.100192	1949716.195040	6534.286157	104	90	95	72
6606185.499840	1949715.864228	6533.970970	110	91	95	78
6606185.659510	1949715.974899	6533.991895	117	74	82	61
6606185.701791	1949715.863111	6534.065486	110	93	98	79
6606186.486480	1949716.083685	6534.182730	123	73	76	57
6606186.900299	1949716.195031	6534.432737	128	73	82	65
6606186.927108	1949715.970407	6534.416317	109	71	77	63
6606186.725250	1949716.083173	6534.327508	125	69	73	58
6606186.888875	1949716.082889	6534.424427	111	60	68	55
6606186.433095	1949715.972173	6534.175321	128	63	66	47
6606186.551008	1949715.858721	6534.399396	111	67	70	57
6606186.581266	1949715.971606	6534.320099	126	62	64	51
6606186.376058	1949715.747392	6534.408007	103	56	65	49
6606185.846893	1949715.974184	6534.083408	119	57	60	44
6606186.226754	1949715.636412	6534.430835	126	61	69	52
6606186.034215	1949715.526320	6534.402700	106	85	89	72
6606186.090653	1949715.861082	6534.207460	118	83	93	69

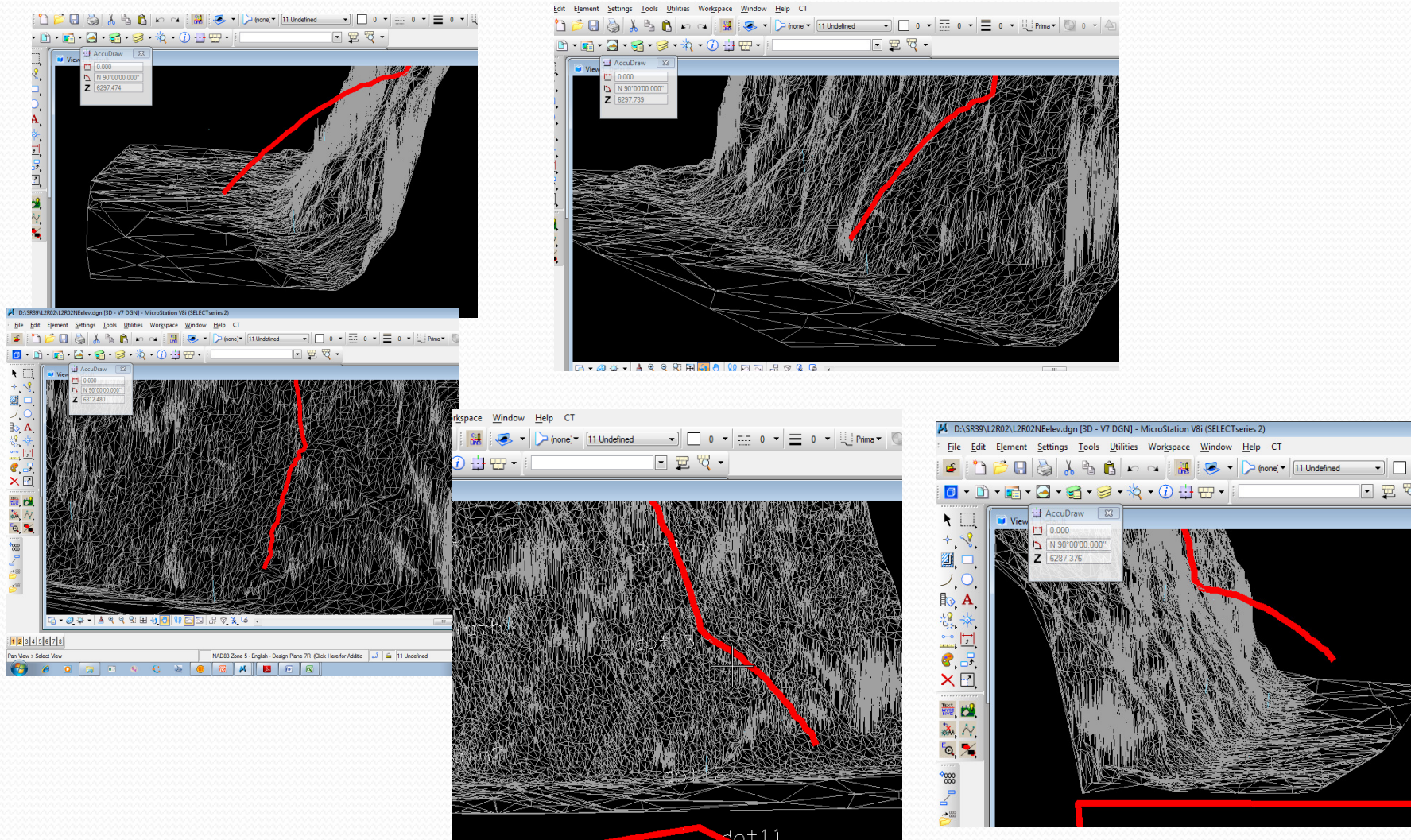
Microsoft Excel 2007 interface showing a spreadsheet with columns A through E. The formula bar displays:  $=DV5\_L2R02\_xyzpts!B2+NEelev\_of$

	A	B	C	D	E
1	Frame	Northing	Easting	Elevation	
47	46	1947113.614	6605849.178	6351.485545	
48	47	1947113.489	6605848.811	6350.224702	
49	48	1947113.506	6605848.265	6348.88058	
50	49	1947113.552	6605847.311	6347.361067	
51	50	1947112.815	6605846.582	6345.889015	
52	51	1947112.507	6605846.268	6344.612238	
53	52	1947112.328	6605845.66	6342.891798	
54	53	1947112.041	6605845.111	6341.363755	
55	54	1947111.695	6605844.367	6339.996927	
56	55	1947111.383	6605843.89	6338.031457	
57	56	1947111.194	6605843.231	6336.659531	
58	57	1947111.136	6605842.58	6334.950012	
59	58	1947110.657	6605842.12	6332.606002	
60	59	1947110.483	6605841.66	6331.181415	
61	60	1947110.349	6605840.875	6329.357613	
62	61	1947110.054	6605840.708	6327.526637	
63	62	1947109.7	6605839.497	6326.315757	
64	63	1947109.366	6605838.675	6325.661064	
65	64	1947109.669	6605836.685	6325.131693	
66	65	1947110.11	6605835.524	6325.096778	
67	66	1947110.276	6605834.619	6324.820101	
68	67	1947110.086	6605833.097	6324.278468	
69	68	1947110.598	6605831.767	6324.054635	
70	69	1947110.611	6605830.564	6323.550386	
71	70	1947111.049	6605829.694	6323.165878	

Ready



# 3-D CAD from Analysis





# Trajectory

- A cross section of rock trajectory from x,y,z positions can provide:
  - Bounce height (i.e. will barriers work)
  - Energy toward impact
  - Calibrate software
  - Determine parameters for simulation
  - Evaluate how aggressive our simulations may be.



# Trajectory and Energy

- Trajectory is determined from frame to frame by:

- Distance:

$$x = \sqrt{\Delta Northing^2 + \Delta Easting^2 + \Delta elevation^2}$$

- The elevation is plotted against distance to make a profile

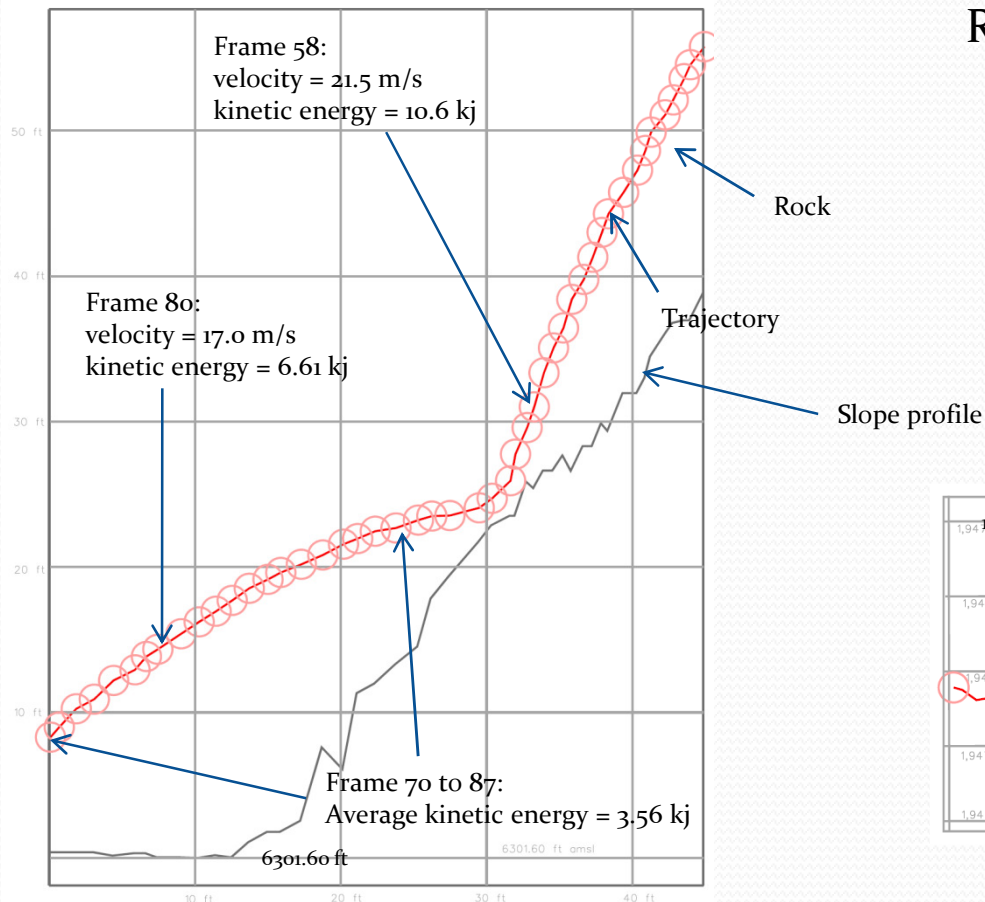
- Energy is determined by:

- Time = 30/1001 seconds
- Speed = Distance/time
- Energy =  $\frac{1}{2}$  mass x speed<sup>2</sup>

# Trajectory Profile and Energy

## Location 2 Rock 2

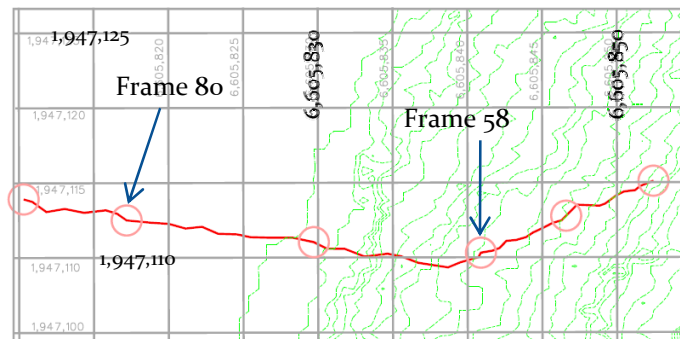
Profile



### Rock Parameters:

- Weight = 101 lbs
  - mass = 3.14 slugs (45.8 kg)
- Initial length = 26 inches
- Initial depth = 17 inches
- Initial width = 7 inches

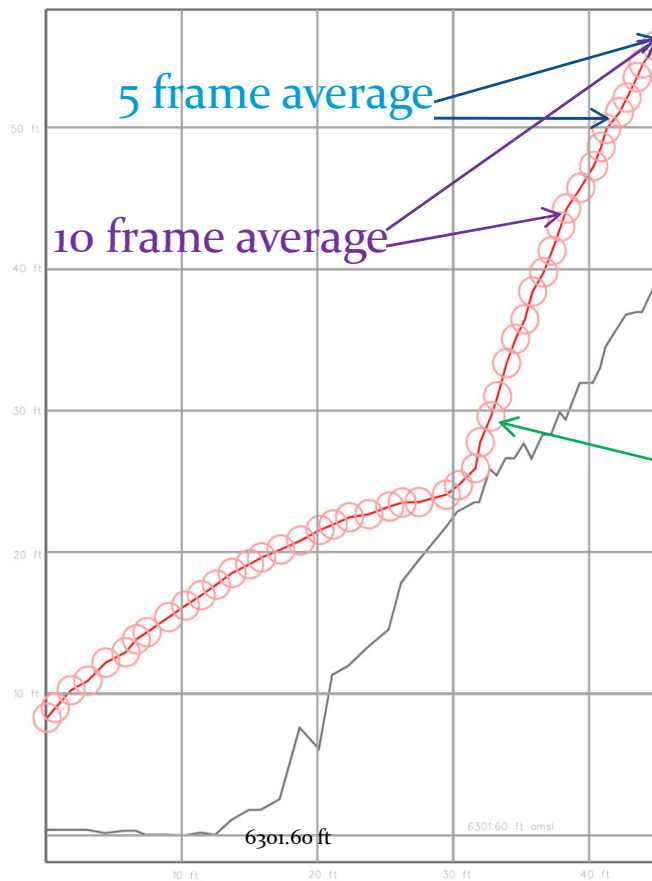
Plan View





# Energy Analysis

Profile

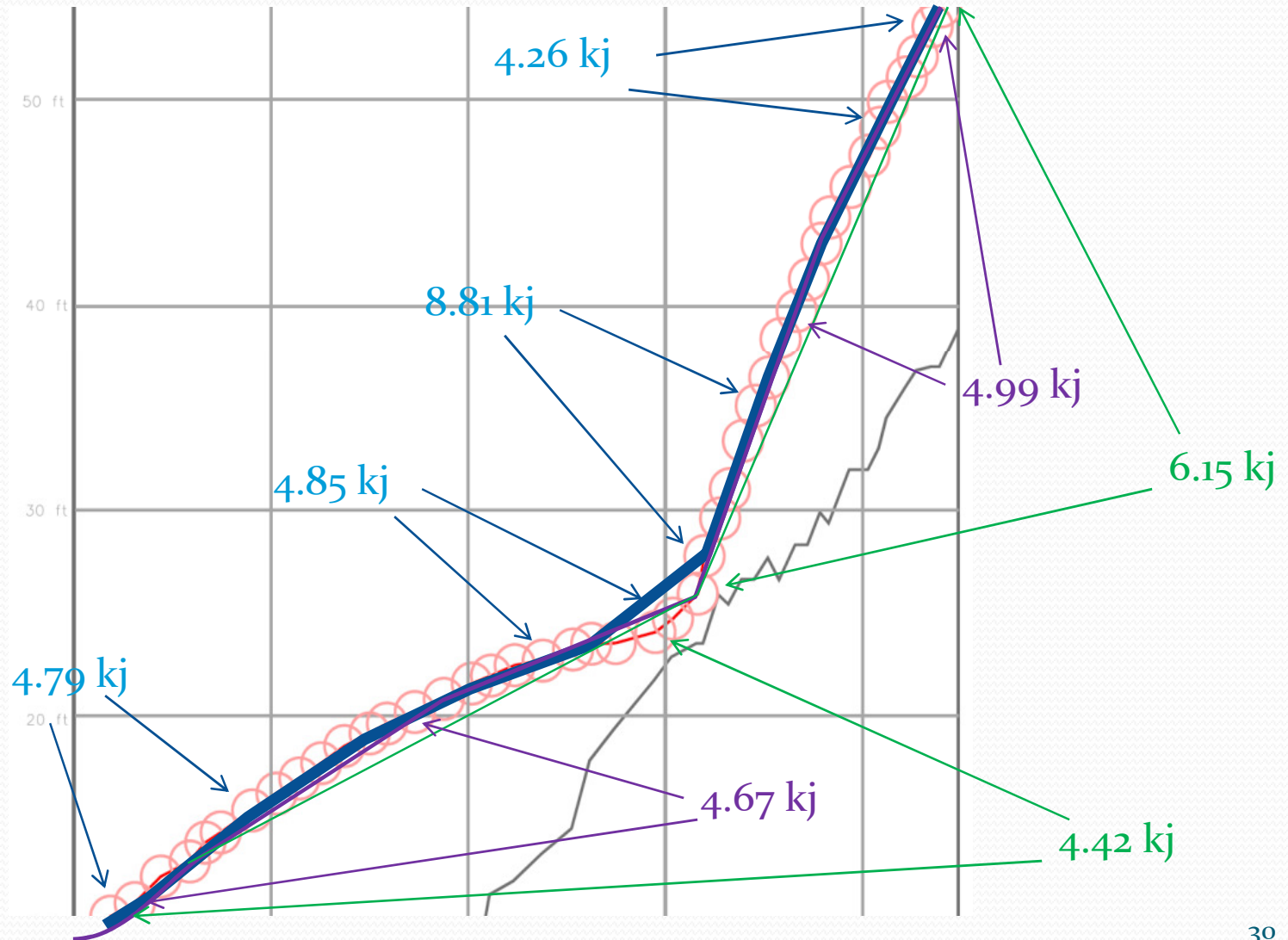


~~$$\frac{\sum x_{\text{frame/frame}}}{\sum \Delta \text{frame} * \frac{30}{1001}} = \text{kinetic energy from frame A to frame B}$$~~

$$\frac{\sqrt{\Delta N_{A \text{ to } B}^2 + \Delta E_{A \text{ to } B}^2 + \Delta \text{elev}_{A \text{ to } B}^2}}{\sum \Delta \text{frame} * \frac{30}{1001}} = \bar{k}$$

20 frame average

# Frame to Frame Energy

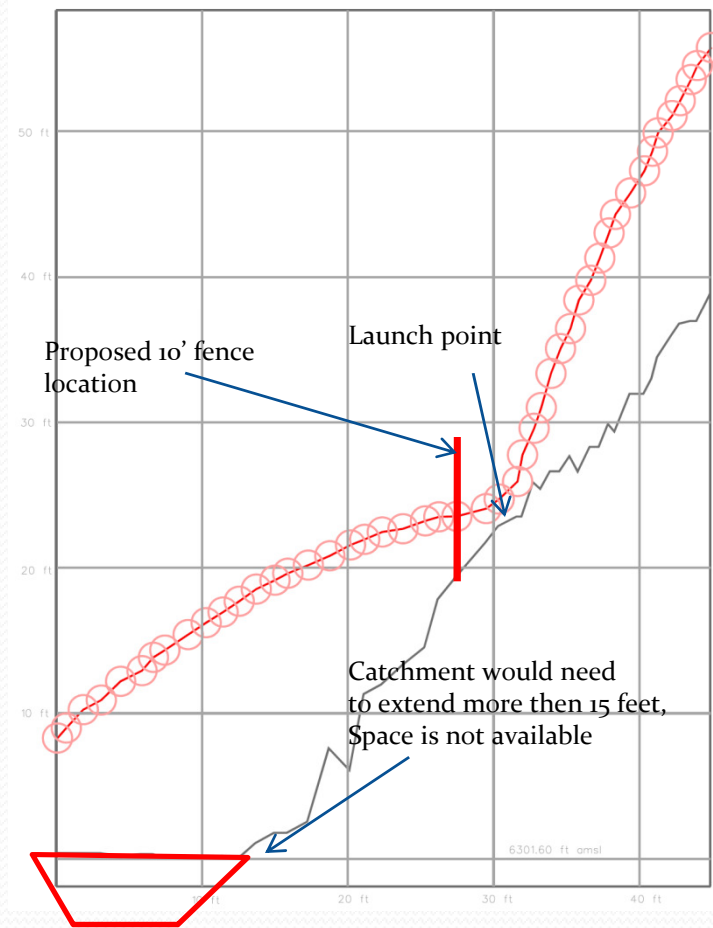


# Field Data compared to Video

## Rock L2R02

Results Based on Field Measurement			<i>Results Based on Video</i>			
PE (kj)	Ave. K (kj)	PE (kj)	Ave. K (kj)			
			total trajectory	last 5 frames	last 10 frames	last 20 frames
14.6	1.2	6.49	5.46	4.79	4.67	4.42

# Results



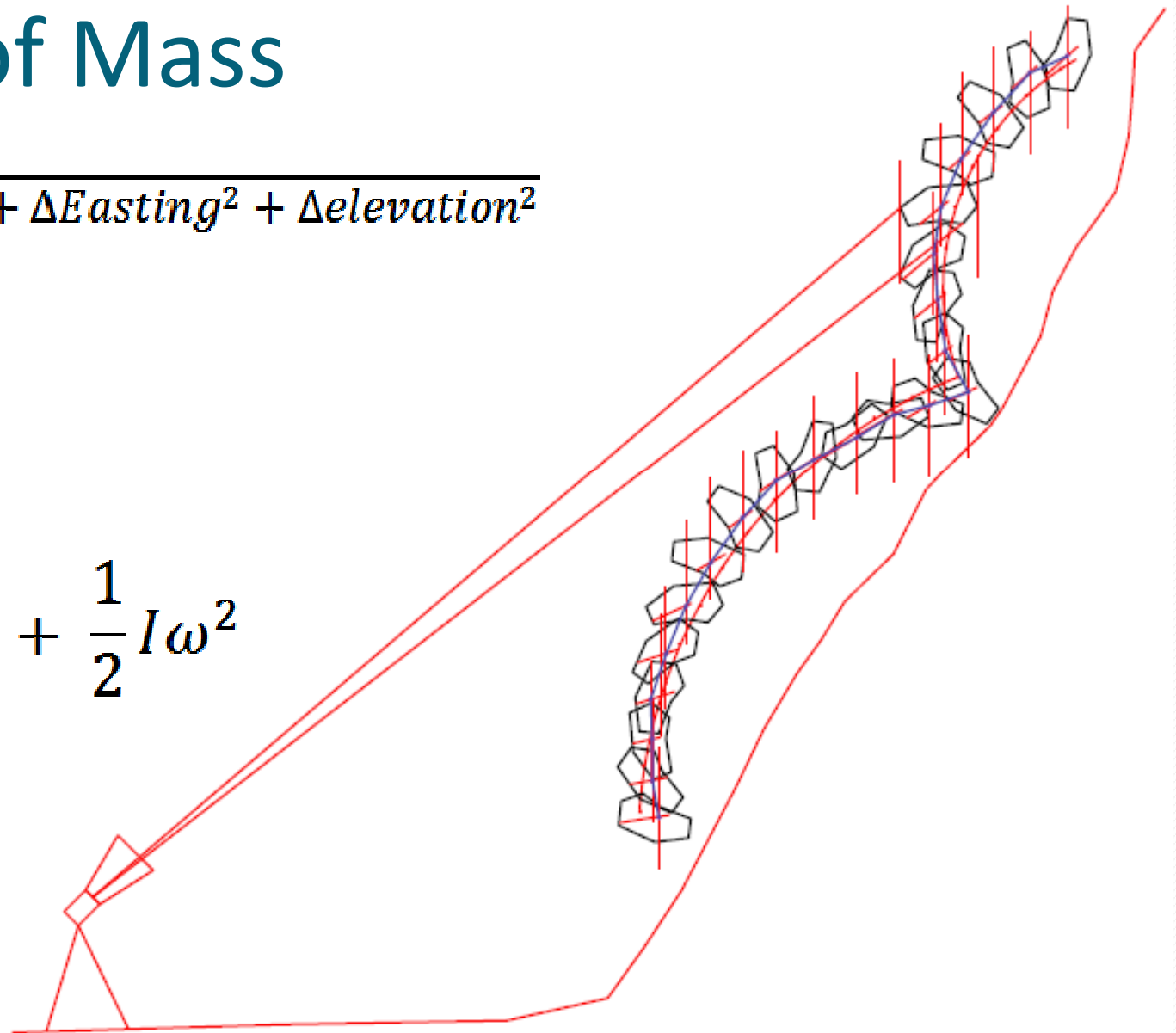
- For location 2 a proposed fence might be placed at the redline
- If other rocks miss this point, a barrier may not be useful here
- Redeveloping a catchment may not be feasible
- Drapery could be a better alternative

# Center of Mass

$$x = \sqrt{\Delta Northing^2 + \Delta Easting^2 + \Delta elevation^2}$$

$$\frac{x}{t} = v$$

$$k = \frac{1}{2}mv^2 + \frac{1}{2}I\omega^2$$



# Center of Mass

elev.xlsx - Microsoft Excel

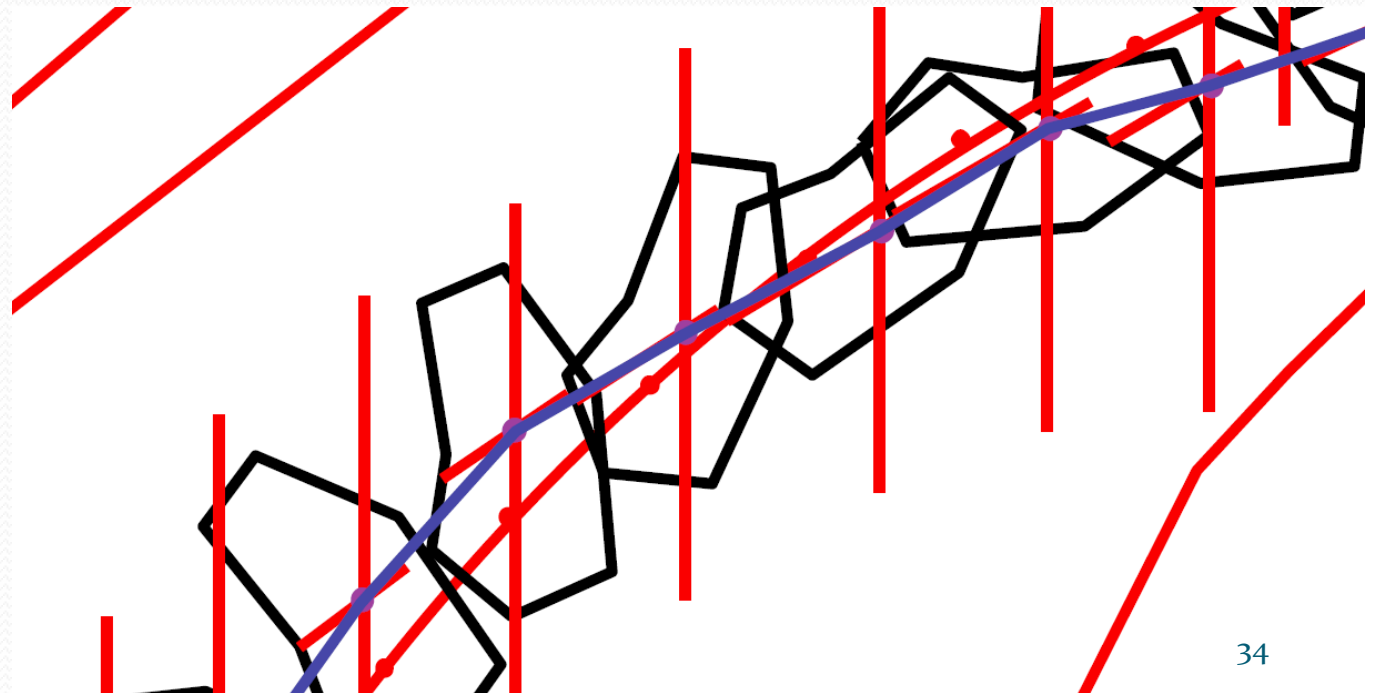
Arrange All Freeze Panes Split View Side by Side Hide Synchronous Scrolling Unhide Reset Window Position Window

	G	H	
/sec	x in meters	v: average speed in m/sec	kinet
	0	#DIV/0!	
188002	0.47764136	13.85159943	
382587	0.320237866	9.286898124	
205492	0.49735529	14.4233034	
141214	0.355506235	10.30968082	
340844	0.464855824	13.48081889	
163786	0.402069435	11.66001362	
182889	0.44222096	12.82440785	
588041	0.54702015	15.86358435	
553302	0.548813768	15.91559927	
708684	0.411554485	11.93508007	
568017	0.558905245	16.20825211	
796447	0.502478192	14.57186757	
545919	0.486066233	14.09592076	
188414	0.623693155	18.08710149	
335888	0.467537857	13.55859787	
300007	0.557815532	16.17665042	
724445	0.742632004	21.53632811	
113229	0.459315973	13.32016322	
157354	0.606568538	17.59048761	
399643	0.567548073	16.45889411	
366981	0.533018157	15.45752656	
114052	0.336132815	9.747851629	
729652	0.634586206	18.40299998	
565431	0.378421843	10.97452243	

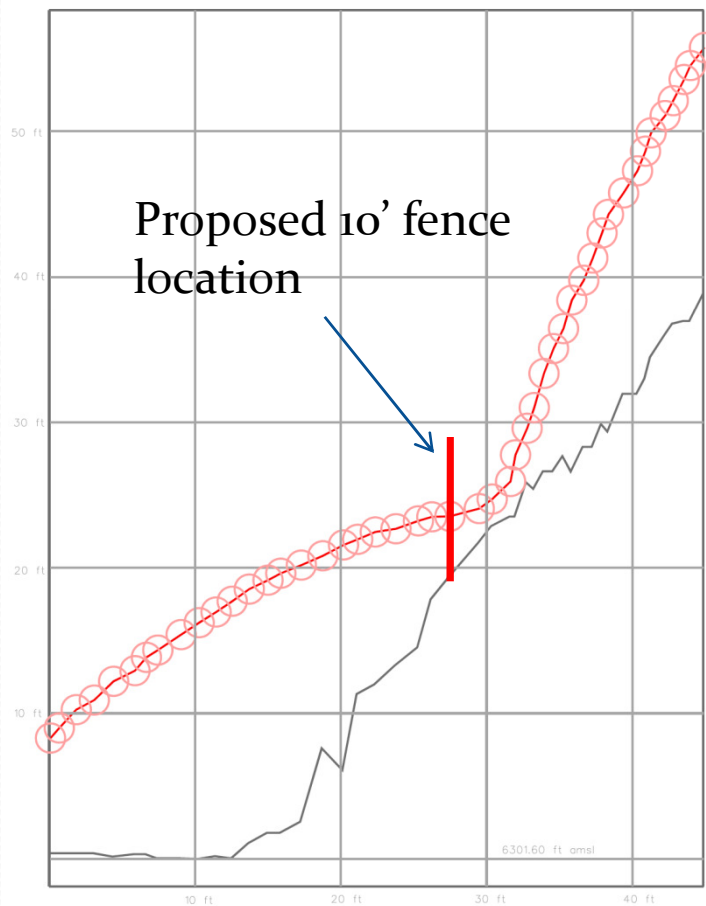
energy

$$\frac{0.4572^m}{0.02997^{sec}} = 15.26^{m/sec} \rightarrow \frac{1}{2} 45.77 \times 15.26^2 = 5.392^{kj}$$

$$\frac{0.1524^m}{0.02997^{sec}} = 5.09^{m/sec} \rightarrow \frac{1}{2} 45.77 \times 5.09^2 = 0.592^{kj}$$



# Conclusions



- Trajectory Profile w/o Energy:
  - We can visualize effectiveness of barriers
  - Determine barrier height
- Trajectory Profile w/ Energy:
  - Provides a conservative estimation of energy